Physical Science International Journal
4(5): 723-733, 2014

SCIENCEDOMAIN ***international***
www.sciencedomain.org

Vibration Technique for Processing and Monitoring Electrical and Mechanical Defects in Electrical Drives Using 2-D Mathematical Model

Ali S. Hennache[1*] and Lazhar Bougoffa[2]

[1]Department of Physics, College of Sciences, Al Imam Mohammad Ibn Saud Islamic University (IMSIU), P.O .Box 90950, Riyadh, 11623, Kingdom of Saudi Arabia.
[2]Department of Mathematics, College of Sciences, Al Imam Mohammad Ibn Saud Islamic University (IMSIU), P.O .Box 90950, Riyadh, 11623, Riyadh, Kingdom of Saudi Arabia.

Authors' contributions

This work was carried out in collaboration between both authors. Author ASH managed the literature searches and placed the research objectives of the paper in perspective, designed the study, wrote the protocol and wrote the first draft of the manuscript. Author LB managed the literature searches, checked and commented on the mathematical model. Both authors read, edit and approved the final manuscript.

Original Research Article

Received 30th June 2013
Accepted 28th February 2014
Published 14th March 2014

ABSTRACT

The radial flux density in the air-gap of rotating machines sets up a force of attraction between the stator and the rotor surfaces. In a symmetrical machine, the radial stresses distributions are balanced resulting in zero net force on the rotor. However, if the rotor of a rotating machine is supported eccentrically with respect to the stator or if rotor short circuits occur, a one-sided magnetic force will be developed which generally tends to increase the eccentricity and increases considerably the critical speed of the machine. The resultant force created by the unbalanced forces of attraction is called unbalanced magnetic pull (ump). Under certain conditions these forces may cause the individual parts of the machine to vibrate and thus develop a noise. The vibrating parts are more stressed and are frequent sources of troubles, they also cause a rapid ageing of the machine. Furthermore, the machine vibrations are transferred to the bases and may, with large machines, cause a vibration of the entire surroundings of the machine. In the following paper a brief outline of the mathematical analysis associated with a technique for monitoring defects in rotating machine whilst the machine is running in normal service is

*Corresponding author: Email: ashennache@imamu.edu.sa;

described. This technique is based upon the use of sensors in the air-gap, so arranged that the symmetrical air-gap is eliminated and only the lack of symmetry due predominantly to the missing flux associated with electrical and mechanical failures (eccentricity, increased vibrations, bending of the rotor shaft etc.), are displayed. A small four-pole machine with a modified field winding and bearings is used to examine experimentally both electrical and mechanical anomalies of various magnitude and position.

Keywords: Synchronous machines; turbogenerators; drive systems; anomalies; monitoring; harmonics; diagnosis.

1. INTRODUCTION

The radial flux density in the air-gap sets up a force of attraction between the stator and the rotor surfaces. In a symmetrical machine, the radial stresses distributions are balanced resulting in zero net force on the rotor. However, when rotor short circuits occur, these latter operate at lower temperatures than coils without shorted-turns. Turns shorted cause an unequal distribution of active turns between poles and thus cause unequal heating of the rotor leading to a magnetic asymmetry in the air-gap. If the percentage of total turns shorted out is small, the generator may be able to run at rated load for long time without further problems. However, when larger shorted-turns occur, they can cause operating conditions that may limit unit loads. Thus, higher field current is required to maintain a specific load. This higher field currents will result in an increase in I^2R loss for the entire rotor winding and thus the total heat generated by the field will be increased when compared to operating at the same load factors without shorted turns. With a magnetic asymmetry in the air-gap, the radial forces of attraction are no longer balanced, and may cause the individual parts of the machine to vibrate and thus develop noise. The resultant force created by the unbalanced forces of attraction is called unbalanced magnetic pull (ump). There are different factors causing unbalanced magnetic pull [1,2], the main one being rotor eccentricity [3].

The field in the air-gap is dependent on the eccentricity [4], which can occur due to inaccurate positioning of the rotor with respect to the stator, mechanical unbalance, bearing and misalignment problems [5,6,7] on the saturation of the stator and on many other factors [1]. Many other works have also looked at the eccentricity as a major cause of the asymmetrical field in the air-gap [8,9,10]. The main results of ump being increased vibrations, increasing bearing load, bending of the rotor shaft etc. However, an electrical breakdown in the rotor winding or in the stator winding, also causes an asymmetry between the poles and can lead to additional ump and vibration [11,12,13,14].

The vibrating parts are more stressed and are frequent sources of troubles, they also cause a rapid ageing of the machine. Furthermore, the machine vibrations are transferred to the bases and may, with large machines, cause a vibration of the entire surroundings of the machine. Taking up the idea that air-gap search coils [15,16] show promise in rotor winding fault detection, a magnetic field analysis model is used in this paper, an expression is obtained for the emf (flux) to be expected from a balanced pair of search coils in the air-gap, so arranged that the symmetrical air-gap is eliminated and only the lack of symmetry due predominantly to the missing flux associated with the shorted turns, or the eccentricity, is displayed. With the addition of a fairly simple circuit the output of such a system of search coils could be continuously monitored and processed and the appearance of a short circuit, or the deterioration of an existing fault or an eccentricity, indicated in some manner. Thus, the basis of this work has been the measurements of flux (voltage) and noise (vibration) quantities by means of search coils in the air-gap. The theoretical emf (flux) is verified by open-circuit measurements on a DC field small four-pole cylindrical rotor synchronous machine with a specially prepared rotor made of mild steel with 24 slots, 142mm long and 184 mm in diameter, with a 5mm air-gap.

The field windings consist typically of three pairs of slots for each pole. Each slot pair contains one concentric coil, which, in one of the poles is divided into 4 smaller coils of 14, 26, 39 and 52 turns. The coil pitches are 30º, 54º and 78º (mechanical) (Fig. 1b). To study the air-gap harmonic frequencies at various values of eccentricity, special bearings were made for both ends of the motor.

2. ANALYTICAL MODEL OF ROTOR INTER-TURN FAULT

The analysis is based on the main assumption of linearity, which neglects the effect of saturation, so that following Ward [17], the field of the missing turns can be analyzed separately. The rotor winding is assumed to be a current sheet on the surface of a smooth cylinder of radius R_1 (Fig. 1a). we consider the fault to be located in one coil of pitch 2α, of the North Pole centered on $\theta = 0$ the rotor slot width is taken to be 2β mechanical radians and the slot current density $b = {}^{I_{dc}T_m}/_{2\beta}$ $(A\,rad^{-1})$where T_m is the number of the missing turns. The equivalent current sheet of the missing ampere-turns is shown [18] to be

$$K_n = -\frac{2I_{dc}T_m}{\pi\beta R_1} . \frac{1}{n} \sin n\alpha \sin n\beta \qquad (1)$$

Since the excitation current K_{zs} on the surface of the rotor flows in the axial direction only, the two-dimensional magnetic field can be expressed in terms of the magnetic vector potential component A_z, where A is defined as:

$$\underline{B} = Curl\,\underline{A}$$

$div\underline{A} = 0$

And so

$$B_r = \frac{1}{r}\frac{\partial A_z}{\partial \theta} \qquad (2)$$

And

$$H = \frac{1}{\mu_0\mu_r}\frac{\partial A_z}{\partial r} \qquad (3)$$

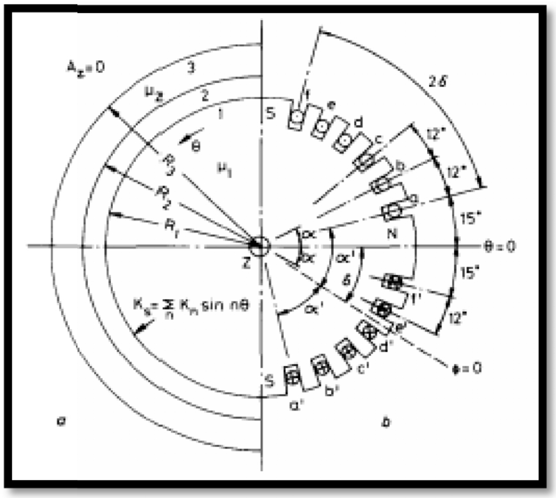

Fig. 1. (a) Analytical model first; (b) Rotor slotting and coils

In the two dimensional polar coordinates in terms of Z component of A

$$\frac{\partial A_z}{\partial r} + \frac{1}{r}\frac{\partial A_z}{\partial \theta} + \frac{1}{r}\frac{\partial A_z}{\partial \theta} = 0. \tag{4}$$

Applying boundary conditions in the air-gap at $r = R_1$ and $r = R_2$and if no flux is allowed to leave the back of the stator core, i.e. there is negligible back-of core leakage flux, then at $r = R_3,\ A_{z_s} = 0$ and so from eqn.4 and if the rotor, with $2p$ poles, runs at ω/p radians per second in the direction of increasing θ, the flux density with respect to the stator has the form

$$B_{r(r)} = \frac{1}{r}\sum_n B_n(r)\cos\left[n\left(\theta - \frac{\omega t}{p}\right)\right]. \tag{5}$$

Suppose there are two identical search coils of span 2γ mechanical radians lying on an $r =$constant plane in the air-gap, one centered on the line $\theta = 0$, and the other on the line $\theta = \pi$. If the search coils are connected in series opposition, as required in a machine with an even number of pole pairs (2,4,6,8,.....) ,the total flux is given by $\varphi^{-} = \varphi_1 - \varphi_2$, with odd values of n. However, if the two search coils are connected in series in the same sense, as required in a machine with an odd number of pole pairs (1,3,5,7,...), the total flux is $\varphi^{+} = \varphi_1 + \varphi_2$, but with even values of n. Thus the general form of the total flux linkage is given by

$$\varphi^{\pm} = \left\{2R_1 \sum_n \frac{X_n}{n}\left[Y_n\left(\frac{R_1}{R_2}\right)\left(\frac{r}{R_2}\right) + \left(\frac{R_1}{r}\right)\right]\sin n\gamma \cos\frac{n\omega t}{p}\right\}.[1 \pm \cos n\pi] \tag{6}$$

And the induced emf has the form

$$e_{\pm} = \frac{4R_1\omega}{p}\ \sum_n X_n\left[Y_n\left(\frac{R_1}{R_2}\right)\left(\frac{r}{R_2}\right) + \left(\frac{R_1}{r}\right)\right]\sin n\gamma \sin\frac{n\omega t}{p}. \tag{7}$$

Where

$X_n = \frac{\mu_0 \ \mu_1}{\mu_1 + 1} \ K_n \left\{ 1 - \frac{\mu_1 - 1}{\mu_1 + 1} \ \left(\frac{R_1}{R_2}\right)^{2n} \ Y_n \right\}, \ Y_n = \frac{\mu_2 \ Z_n - 1}{\mu_2 Z_n + 1}$ and

$$Z_n = \frac{\left\{1 - \left(\frac{R_2}{R_3}\right)^{2n}\right\}}{\left\{1 + \left(\frac{R_2}{R_3}\right)^{2n}\right\}}$$

For the special case of search coils positioned at the stator bore (r = R_2) with four pole machine.

$$e_{-} = \frac{4R_2\omega}{p} \sum_n \left(\frac{R_1}{R_2}\right)^a X_n (Y_n + 1) \sin n\gamma \sin \frac{n\omega t}{p}. \tag{8}$$

Where $a = n + 1.$

A more detailed solution is given by [18].

3. ANALYTICAL MODEL OF STATIC ECCENTRICITY

If the rotor of a synchronous machine is supported in its bearings eccentrically with respect to the stator, a one-sided magnetic force will be developed which generally tends to increase the eccentricity and may cause the individual parts of the machine to vibrate and thus develop noise and increases considerably the critical speed of the machine, and it is obvious that a decisive reason for noise creation is the vibration of the active stator iron.

If R_1 and R_2 denote the rotor and the stator radii, respectively, the rotor eccentricity with respect to the stator is Eg where $g = R_2 - R_1$is the mean air-gap and E is the fractional eccentricity less than unity. The actual air-gap g as a function of the angle θ for a rotor offset by distance Eg is given by

$$g' = g + Eg \ \cos\theta \tag{9}$$

Where $\theta = 0$ is the line of the largest and smallest air gap If $E \ll 1$, then the air-gap permeance is given by

$$\lambda = \frac{1}{g'} = \left[\frac{1}{g(1+E\cos\theta)}\right] = \frac{1-E\cos\theta}{g} \tag{10}$$

In a machine with p pole pairs, and if the excitation is provided by a three phase stator winding static eccentricity will add two-adjacent harmonics of order $ip \pm 1$ reduced in magnitude by a factor $E/_2$.

If the excitation is provided by dc winding on the rotor, i.e. we have a synchronous machine on open circuit; the mmf with respect to the stator is of the form.

$$F(\theta) = \sum_i F_i \cos ip\left(\theta - \frac{\omega t}{p}\right). \tag{11}$$

Both the fundamental and all odd harmonics rotate at synchronous speed, i.e. at $\frac{\omega}{p}$ radians/second (mechanical). The i th radial flux density harmonic now produces as a result of static eccentricity.

$$B_{r_i} = \frac{\mu_0 F_i}{\theta}\left[\cos(ip\theta - i\omega t) - \frac{E}{2}\{\cos(ip+1)\theta - i\omega t + \cos(ip-1)\theta - i\omega t\}\right] \quad (12)$$

Thus, whereas, the fundamental excitation from both stator and rotor sources, and all harmonics present in the stator field, induce 50 Hz emfs in coils stationary with respect to the stator, the rotor harmonics induce 50 iHz emfs in the same coils. This is important from the point of view of air-gap search coils used for the detection of rotor short circuits.

Since $(\theta) = \int K(\theta)R_1 d\theta$, where $K(\theta)$ is the current density distribution on the surface of the rotor, we require $K(\theta)$ for a concentric rotor winding as

$$K(\theta) = \frac{2I_{dc}T_t}{\pi\beta R_1}\sum(-1)\sin(ip\beta)\,\mathrm{K_p}\cos(ip\theta) \quad (13)$$

Where T_t is the total number of conductor per slot.

Where $K_p = \frac{\sin\left(\frac{1}{2}M\ ipT_s\right)}{\sin\left(\frac{1}{2}\ ipT_s\right)}$.

Returning to the notation in terms of the integer n, we have $ip = n$ and $i = {}^{n}/_{p}$ so that

$$F(\theta) = -\frac{2I_{dc}T_t p}{\pi\beta}\sum\left(\frac{1}{\mathrm{n}^2}\right)(1)^{\mathrm{a}}\sin(n\beta)\frac{\sin\frac{1}{2}MnT_s}{\sin\frac{1}{2}nT_s} \quad (14)$$

Where $a = \frac{n}{p} - 1$.

T_s is the slot pitch (displacement angle of the coil in the positive $\emptyset$ direction), and M the number of slots per pole or in other words the number of coils per pole pair. After some work we finally obtain the instantaneous emf induced in the air-gap search coils by any rotor winding harmonic as

$$e_{-} = -4rD_n\frac{\omega}{p}\sum_n\left[\frac{E\sin(n+1)\gamma}{2(n+1)} + \frac{E\sin(n-1)\gamma}{2(n-1)}\right]\sin\frac{n\omega t}{p} \quad (15)$$

Where r is the radius of the search coil position in the air-gap and D_n is given by

$$D_n = -\frac{\mu_0}{8}\frac{2I_{dc}T_t p}{\beta}\frac{1}{n^2}(-1)^{a_1}\sin(n\beta)\frac{\sin\frac{1}{2}M_nT_s}{\sin\frac{1}{2}nT_s}$$

And $a_1 = \frac{1}{2}\left(\frac{n}{p} - 1\right)$.

4. THEORETICAL AND EXPERIMENTAL RESULTS

Theoretical and experimental EMFs from a diametrically opposite set of single-turn search coils on the stator surface are presented in Table 1 for a field current of *2A,* a relative permeability of 800, and a search coil width of 21 mm (12.4º) for different percentage fault in different coil of different pitches. Fig. 2 shows the theoretical EMF when 52 turns (40% of slot contents) are omitted from the concentric coil of pitch 54º. The horizontal time axis has been converted into mechanical degrees, the one revolution shown representing 40 ms for the four-pole machine operating at 50 Hz. The location of the fault can be found by measuring the distance between adjacent positive and negative peaks.

Table 1. Peak values of EMF (mV) produced by different faults

Missing Turns (%)	Pitch of Faulty Coil					
	30º		54º		78º	
	Theory	Exp.	Theory	Exp.	Theory	Exp.
10.7	14.2	16.8	14.2	15.4	14.2	13.0
19.8	26.6	28.5	26.4	27.7	26.4	25.8
29.8	39.9	38.4	39.8	33.2	39.6	39.8
39.7	53.3	50.1	53.0	54.0	52.3	53.4

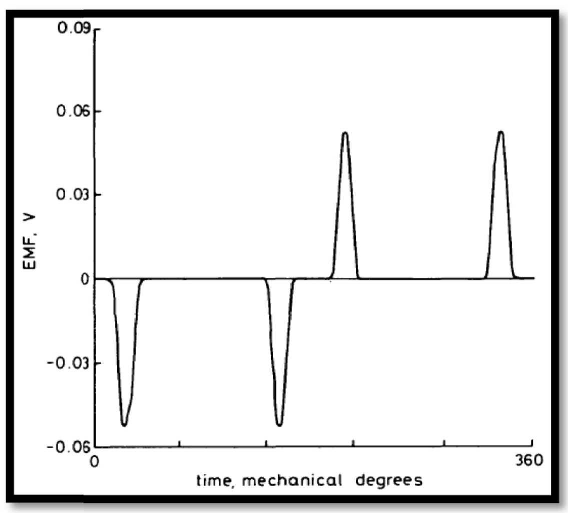

Fig. 2. Predicted EMF waveforms for 4-pole machine with 52 turns (40% of slot contents) omitted from concentric coils of pitch 54º

The search coil analogue data from the experiments (after amplification) was filtered and subjected to spectral analysis. A suite of programs in the microcomputer controls the analyzer and presents the processed data to the experimenter in graphical or numerical forms. Fig. 3 shows the experimental output waveform from one pair of search coils of 24.8º pitch with 40% (52 turns) loss of turns in the concentric coil of pitch 54º.

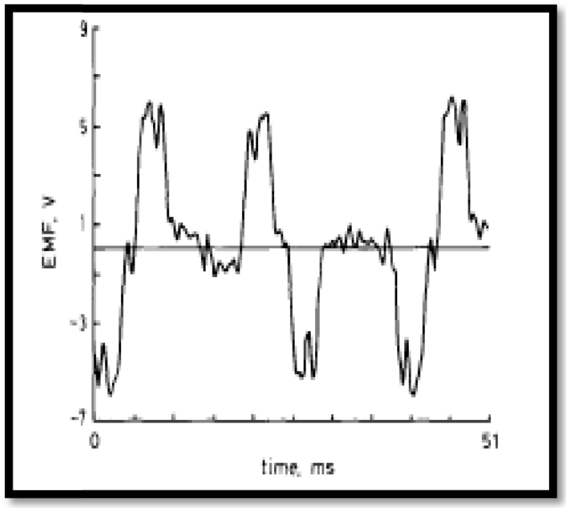

Fig. 3. Experimental EMF waveform from 4-pole machine with 40% fault in one field coil of pitch 54º and no eccentricity (Gain 100)

In the presence of static eccentricity (20%) emf is only induced in the search coils by harmonic pairs of order n +1 at odd multiples of 50 Hz, i.e. 50, 150, 250, 350 etc. (Fig. 4).

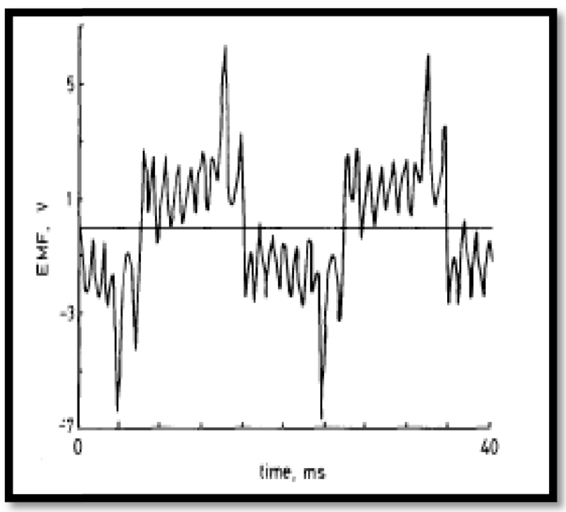

Fig. 4. Experimental EMF with 20% eccentricity and no shorted turns (Gain 100)

Attempting to see how the harmonic spectrum changes as function of static eccentricity, Table 2 was compiled for representative harmonics, and from this resume of results it is clear that the larger the eccentricity, the greater the magnitude of odd multiples of 50 Hz. Thus, it turns out that at least the important lower eccentricity harmonics (odd multiples of 50 Hz such as 50Hz, 150 Hz, 250 Hz etc.) are produced in approximate proportion to the degree of static eccentricity. On the other hand, the harmonics expected from the constant winding fault (odd multiples of 25 Hz such as 25 Hz, 75Hz, 125 Hz etc.) are reasonably constant and the small variation present has no particular pattern.

Table 2. Harmonic magnitudes in volts as a function of eccentricity in the presence of 40% fault in 30º coil

Frequency	Eccentricity (mm)		
Hz	**0 (0%)**	**1 (20%)**	**2 (40%)**
25	0.0031	0.0035	0.0037
50	0.0027	0.0161	0.0464
75	0.0093	0.0079	0.0101
125	0.0121	0.0135	0.0132
150	0.0009	0.0098	0.0204
175	0.0101	0.0107	0.0120
225	0.0075	0.0065	0.0081
250	0.0007	0.0065	0.0142

Table 2 was compiled for representative harmonics and from this resume of results it is clear that the larger the eccentricity, the greater the magnitude of odd multiples of 50 Hz. Thus, it turns out that at least the important lower eccentricity harmonics (odd multiples of 50 Hz) are produced in approximate proportion to the degree of static eccentricity. On the other hand, the harmonics expected from the constant winding fault (odd multiples of 25 Hz) are reasonably constant and the small variation present has no particular pattern. Thus, although the visual distortion can be very severe, the winding fault harmonics are clearly preserved.

We have seen in Fig. 2, measuring the distance between adjacent peaks in the EMF waveform (Table 1) derived from the difference field is a sensitive way of determining the faulty coil. However, eccentricity may distort the signal to be expected from a rotor winding fault. This will, at least, make the measurement of the peak to peak distance more difficult. A helpful way to proceed is to examine the harmonic spectra of rotor short circuits and rotor eccentricity, in the hope that each fault will have a substantially different spectrum.

Table 3 lists the harmonic content produced by a 40% loss of turns in the concentric coils of pitch 30º, 54º and 78º. It can be seen that some of the harmonics change significantly with fault position: for example, as the coil pitch increases the first frequency (25 Hz) increases but the 125 Hz component decreases.

Table 3. Harmonic magnitudes (V) produced by rotor winding fault (40% omitted) and static eccentricity

Frequency Hz	Rotor Winding Fault in						10% Static Eccentricity
	30ºCoil	**54ºCoil**	**78ºCoil**	**30ºCoil**	**54ºCoil**	**78ºCoil**	
	Predicted			**Experimental**			
25	0.00358	0.00627	0.00871	0.00359	0.00570	0.00764	------------
50	----------	----------	----------	0.00316	0.00298	0.00289	0.00347
75	0.01017	0.01420	0.01281	0.00102	0.00124	0.00120	------------
125	0.01335	0.00977	0.00358	0.00124	0.00666	0.00160	------------
150	----------	----------	----------	0.00102	0.00105	0.00174	0.00702
175	0.01246	0.00202	0.01288	0.00116	0.00037	0.00762	------------
225	0,00829	0.01045	0.00183	0.00675	0.00617	0,00102	------------
250	-----------	----------	----------	0.00068	0.00124	0.00108	0
275	0.002683	0.09924	0.00968	0.00149	0.00595	0.00758	------------

From the above results. It is worth investigating the use of only two harmonics in this process. The most important piece of information is that a fault is present in a given coil of a concentric group. Now an individual harmonic is approximately proportional to fault magnitude but when assuming linearity the ratio of two harmonics will be very insensitive to that magnitude and to the field current value, but If such ratio vary monotonically with the pitch of the faulty coil then we have a means of determining the fault location. Provided the machine is modeled analytically to find at least one ratio that varies strongly with fault position.

5. CONCLUSION

The double search coil method of detecting anomalies in rotating machines has been shown to work well with rotor shorted turns on no load and low load: not only does the output waveform of the search coils indicate the pitch of the concentric coil in which the fault exists but a relatively simple analytical model of the machine under investigation can give a fairly accurate estimate of the number of turns involved if the peak amplitude is measured. However, with double fault in the system (shorted turns and eccentricity) the system may lead to the possibility of a false indication.

In view of the contamination of sensors output voltage waveforms by different effects, it is worth investigating the harmonic spectrum of different types of fault, in the anticipation that each fault will have a unique spectrum and the information obtained in the simulation could be used to develop a knowledge-based system, which is capable of identifying the location and the nature of the fault through a certain frequency pattern. It is clear that the ratio of two harmonics when it varies monotonically with the pitch of the faulty coil would certainly locate the position of the fault. This ratio looks promising when taking a rotor-winding fault only. It is interesting therefore to see whether this ratio will be sensitive with the presence of other type of faults such as faults in stator part, in the inverter system part or in the rectifier system part. The selection of only two harmonics without a model will merely produce a fault present alert. Thus, further work on an accurate model may also be needed on harmonics ratios to detect the fault position.

COMPETING INTERESTS

Author has declared that no competing interests exist.

REFERENCES

1 Binns KJ, Dye M. Identification of principal factors causing unbalanced magnetic pull in cage induction motors. Proc IEE. 1993;120(3):349-354.

2 Andrej Burakov, Antero Arkkio, Comparison of the unbalanced magnetic pull mitigation by the parallel paths in the stator and rotor winding. IEEE Transactions on Magnetics. 2007;43:12.

3 Faiz J, Ebrahimi BM. Static eccentricity fault diagnosis in an accelerating no-load three-phase saturated squirrel-cage induction motor.Progress in Electromagnetics Research B. 2008;10:35–54.

4 Swann SA. Effect of rotor eccentricity on the magnetic field in the air-gap of a non-salient pole machine. Proc IEE. 1983;11(5):903-915.

5 Vas P. Parameter estimation, condition monitoring and diagnosis of electrical machines. Clarendron Press, Oxford; 1993.

6 Nandi S, Toliyat HA, Li X. Condition monitoring and fault diagnosis of electrical machines-a review. IEEE Transactions on Energy Conversion. 2005;20(4):719-729.

7 Kiani M, Lee WJ, Kenarangui C, Fahimi B. Detection of rotor faults in synchronous generators. IEEE; 2007.

8 Wang L, Cheung RW, Ma Z, Ruan J, Ying Peng. 'Finite-element analysis of unbalanced magnetic pull in a large hydro-generator under practical operations. IEEE Transactions on Magnetics. 2008;44(6):1558–1561.

9 Perers R, Lundin U, Leijon M. Saturation effects on unbalanced magnetic pull in a hydroelectric generator with an eccentric rotor. IEEE Transactions on Magnetics. 2007;43(10):3884–3890.

10 De Canha D, Cronje WA, Meyer AS, Hoffe SJ. Methods for diagnosing static eccentricity in a synchronous 2 pole generator. IEEE Conference of Power Technology, Lausanne, Switzerland. 2007;1–5:2162–2167.

11 Rahman MKM, Azam T, Saha SK. Motor fault detection using vibration patterns. Electrical and Computer Engineering (ICECE), International Conference. 2010;18-20:486-489.

12 Sadoughi A, Jafarboland M, Tashakkor MS. A practical bearing fault diagnosing system based on vibration power signal autocorrelation. International Review of Electrical Engineering (IREE). 2010;5(1):148-154.

13 Patel RK, Agrawal S, Joshi NC. Induction motor bearing fault identification using vibration measurement. Engineering and Systems (SCES), Students Conference. 2012;16-18:1-5.

14 Cameron JR, Thomson WT. Vibration and current monitoring for detecting air-gap eccentricity in large induction motors. Int Conf on Electrical Machines Design and Applications, London. 1993;173-179.

15 Conolly HM, Lodge I, Jackson RJ, Roberts I. Detection of interterm faults in generator rotor winding using air-gap search coils. Proc Int Conf on Electrical Machines Design and Applications, IEE, London. 1995;11:15.

16 Wood JM, Hindmarsh RT. Rotor winding short detection. Proc IEE. 1986;133(3):181-189.

17 Ward DM. Unbalanced magnetic forces on a two-pole alternator rotor with shorted turn. Proc 19th Universities Power Eng Conf, Dundee, UK; 1994.

18 Hennache Ali. Fault diagnosis through magnetic field pattern recognition in drive systems. Proceedings of the International Conference on Mathematical Applications in Engineering (ICMAE'10) "Engineering Mathematics without bounds", Kuala Lumpur, Malaysia. 2010;3:5.

Peer-review history:
The peer review history for this paper can be accessed here:
http://www.sciencedomain.org/review-history.php?iid=428&id=33&aid=4003